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- Toroidal devices need a rotational transform so that the ∇B drift doesn't lead to charge separation
- In tokamaks, this is provided by a toroidal current, some of which needs to be driven using transformer action, radio waves or neutral beams
- Particle trapping (neoclassical effects) lead to the bootstrap current, which can provide much of the toroidal current
- The distributon of toroidal current has important effects on plasma performance and stability
- In this lecture we'll look at other ways to produce a rotational transform without a toroidal current

It can seem counter-intuitive that you could create a toroidal machine with rotational transform without having a plasma current

- As an example, consider the first such design
- Proposed in 1951 by Lyman Spitzer, Jr^{1 2}
- Called a stellarator since it was inspired by the sun





¹Project Matterhorn. Declassified, renamed PPPL in 1961 ²L.Spitzer, Jr "The Stellarator Concept" IAEA conference 1958. Available from http://www-naweb.iaea.org/napc/physics/2ndgenconf













- In the figure of eight design, field-lines are shifted by an angle of 4α each time they go around the machine. This shift is the rotational transform
- As in a tokamak, this leads to the formation of flux surfaces

Producing rotational transform

- The first designs like the racetrack demonstrate the principle, but did not have very good confinement: they turned out to be unstable with a finite plasma pressure.
- They are complicated to build, and the fields from neighbouring coils tended to interfere with each other

Producing rotational transform

- The first designs like the racetrack demonstrate the principle, but did not have very good confinement: they turned out to be unstable with a finite plasma pressure.
- They are complicated to build, and the fields from neighbouring coils tended to interfere with each other
- There are three ways to get a rotational transform in toroidal devices:
 - A toroidal current, either driven externally or by the Bootstrap current (i.e. tokamak-like)
 - A deformation in 3D (torsion) of the magnetic axis, as in the racetrack machine
 - Non-circular deformation of the magnetic surfaces in resonance with magnetic field lines

Helical Axis Stellarators

To produce a twist in the magnetic axis, draw a helical path, then position the toroidal field coils perpendicular to this path. This produces a configuration called a Helical Axis stellarator, or **Heliac**



Figure : Heliac configuration produced by displacing toroidal field coils³

³A.H.Boozer, Phys. Plasmas **5**, 1647 (1998)

Classical Stellarators

Rather than twisting the magnetic axis, so-called **classical stellarators** deform the flux surface shape by adding helical coils with currents in alternating directions (so field cancels out on axis).



STELLARATOR (2=3)

l = 3 stellarator with 2l = 6 helical windings^a

^aR.L.Miller, R.A.Krakowski LANL report LA-8978-MS (1981)



The original very poor pe subsequent this: the We W-7A at Ma

Heliotrons

Following declassification of fusion research in 1958, stellarator research started in Japan. An alternative design to the classical stellarator was developed⁴ which uses only half the number of coils, all carrying current in the same direction



HELIOTRON (2:3) Figure : R.L.Miller, R.A.Krakowski LANL report LA-8978-MS (1981)



- Heliotrons are easier to build since fewer coils, and the forces between them are reduced
- The Large Helical Device (LHD) is of this design

⁴K.Uo, J. Physical Soc. Japan **16**(7):1380 (1961)

- The helical coils in classical stellarators, heliotrons and variants are hard to build, because they are interlocking, and inside the toroidal coils
- Plot the currents in these coils as a function of θ and ϕ



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- Plot the currents in these coils as a function of θ and ϕ
- Replace with an essentially equivalent set of modular coils



Figure : R.L.Miller, R.A.Krakowski LANL report LA-8978-MS (1981)

Modular coils were a big breakthrough in stellarator design

• Coils can be independently built and then assembled. Design is more difficult, but result is more practical for large reactors



N/m=3 COILS PER FIELD PERIOD

Figure : R.L.Miller, R.A.Krakowski LANL report LA-8978-MS (1981)

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Figure : Wendelstein 7-X under construction, 2010

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Figure : Wendelstein 7-X nearly finished, October 2013

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- Coils can be independently built and then assembled. Design is more difficult, but result is more practical for large reactors
- More importantly, using modular coils allows stellarators to be designed "plasma first", rather than "coil first" ⁵. We can design the plasma equilibrium based on physics considerations, and then design a set of coils to produce the required field.
- Stellarators designed this way are called advanced stellarators, the first example of which was Wendelstein 7-AS.
- Performing and optimising these designs has only become possible with advances in computing power

⁵R.F.Schmitt PhD thesis, Columbia U. 2008

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- As in a tokamak, particles can be passing or trapped due to toroidicity
- There are also particles which get trapped in local minima

- These particles trapped in local minima are confined to regions on the upper or lower half of the flux surface ⇒ their vertical ∇B drift doesn't cancel out, and they drift straight out of the machine. Called super-banana or direct loss orbits ⁶
- This drift is different for electrons and ions, and so leads to electric fields.
- The same process can happen in tokamaks due to toroidal ripple produced by a limited number of toroidal field coils
- This direct loss lead to pretty poor performance in the 1960s and interest moved to tokamaks

⁶J.R.Cary, C.L.Hedrick, J.S.Tolliver, Phys. Fluids **31**, 1586 (1988)

Particle orbits in a tokamak revisited

So why do particle orbits stay near flux surfaces in tokamaks?

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So why do particle orbits stay near flux surfaces in tokamaks?

Consider the toroidal angular momentum of a particle in a tokamak Rv_{ϕ}

$$mrac{d}{dt}\left(R \mathbf{v}_{\phi}
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Using the expressions for an axisymmetric poloidal field

$$\begin{split} \underline{B}_{\theta} &= \nabla \psi \times \nabla \phi \qquad \underline{v} \times (\nabla \psi \times \nabla \phi) = \nabla \psi \left(\underline{v} \cdot \nabla \phi \right) - \nabla \phi \left(\underline{v} \cdot \nabla \psi \right) \\ &\Rightarrow m \frac{d}{dt} \left(R v_{\phi} \right) = -q \underline{v} \cdot \nabla \psi \end{split}$$

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Canonical momentum

- $p_{\phi} = mRv_{\phi} + q\psi$ is called the **canonical momentum**, and is conserved in an axisymmetric configuration
- In lecture 3, we derived an expression for the width of a banana orbit by considering the bounce time and ∇B drift velocity
- An alternative way is to consider the change $\left|\delta\psi\right|\sim\left|\nabla\psi\right|\delta r_{b}$
- This gives an upper bound on the particle orbit width

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A more elegant way to derive the canonical momentum is through the particle Lagrangian. Symmetries lead to conserved quantities, and in this case axisymmetry in a tokamak leads to conservation of canonical momentum

 \Rightarrow Toroidal symmetry leads to a limit on how far particles can deviate from flux surfaces without collisions.

Quasi-symmetric stellarators

- In classical stellarators, there is no toroidal symmetry. Hence canonical momentum is not conserved, and there is no bound on particle excursions from a flux surface.
- Quasi-symmetric stellarators^{7 8} aim to introduce a new symmetry angle and so a canonical momentum

⁷A.H.Boozer, Phys. Fluids **26**(2):496-499 (1983)
 ⁸J.Nuhrenberg and R.Zille, Phys. Lett. A **129**, 113 (1988)

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- In these designs, |B| a function of only ψ and a linear combination $M\theta N\phi$ (in Boozer coordinates)
 - When N = 0, the field has Quasi-Axial Symmetry (QAS)
 - When M = 0, the field has Quasi-Poloidal Symmetry (QPS)
 - When M = 1 and $N \neq 0$ then the field has Quasi-Helical Symmetry (QHS)
- In this case there is a symmetry direction, and a conserved canonical momentum. This leads to a limit on the deviation of particles from flux surfaces, and the same toroidal neoclassical theory applies

⁷A.H.Boozer, Phys. Fluids **26**(2):496-499 (1983)
 ⁸J.Nuhrenberg and R.Zille, Phys. Lett. A **129**, 113 (1988)

Helically Symmetric eXperiment



Figure : HSX
http://www.hsx.wisc.edu

- Helically symmetric stellarator, constructed at Wisconsin as first test of quasi-symmetry
- Began operation in 1999
- Major radius 1.20m, minor radius 0.15m
- Confirmed reduction of direct loss orbits

NCSX



Figure : National Compact Stellarator eXperiment at PPPL http://ncsx.pppl.gov/

- Low aspect-ratio, high performance (β) machines called "compact stellarators" have been designed
- At low aspect-ratio, quasi-helicity cannot be attained^a
- Instead, another symmetry can be used such as quasi-axisymmetry
- Major radius 1.42m, minor radius 0.33m

^aD.A.Garren, A.H.Boozer, Phys. Fluids B 3:2822 (

Note: The NCSX project was mothballed in 2008

A second way to reduce neoclassical transport in stellarators is to make the radial particle drift average out over a bounce orbit.

- These are called omnigenous or linked mirror designs ⁹¹⁰, and need not be symmetric
- The bounce-averaged radial drift can be minimised for a chosen population of particles (i.e. super-bananas), hence the "quasi-"

⁹L.S.Hall, B.McNamara, Phys. Fluids **18**:552 (1975) ¹⁰H.E.Mynick, T.K.Chu, A.H.Boozer Phys. Rev. Lett **48**(5):322 (1986) A second way to reduce neoclassical transport in stellarators is to make the radial particle drift average out over a bounce orbit.

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- The bounce-averaged radial drift can be minimised for a chosen population of particles (i.e. super-bananas), hence the "quasi-"
- The variation in field-strength ∇B within a flux surface is proportional to the curvature
- Since super-banana particles are trapped in regions of low *B*, minimise the curvature in these regions, and put the curvature needed to bend plasma into a torus in regions of high *B*

 ⁹L.S.Hall, B.McNamara, Phys. Fluids 18:552 (1975)
 ¹⁰H.E.Mynick, T.K.Chu, A.H.Boozer Phys. Rev. Lett 48(5):322 (1986)

Wendelstein 7-X

A large Quasi-Omnigenous stellarator being built at IPP Greifswald





Figure : A.H.Boozer, Phys. Plasmas **5**(5):1647 (1998)

- Straight sections with triangular cross-section and low *B*, and curved sections with crescent cross-sections and high *B*.
- Major radius 5.5m, minor radius 0.52m, magnetic field 3T
- Expected to have JET-like plasma performance, and discharge length of \sim 30 minutes
- Planned completion date 2014 at cost of \sim \$300 million

Stellarator equilibria

Stellarator equilibria are quite different to a tokamak:

- In some ways it is easier: currents in the plasma are usually optimised to be small, so the coil currents alone determine the equilibrium
- The Grad-Shafranov equation cannot be used, so now the full 3D $\underline{J} \times \underline{B} = \nabla P$ must be solved. Two codes which do this are VMEC¹¹ and PIES¹²



Figure : W7-X coils: M. Drevlak et al. Nucl. Fusion 45, 731 (2005)

¹¹S.P. Hirschman, *et al.* Phys. Fluids 26, 3553 (1983)
 ¹²A. Reiman and H.S. Greenside, Comput. Phys. Commun. 43, 157 (1986)
 Dr Ben Dudson Magnetic Confinement Fusion (20 of 23)

Optimising Stellarators

Stellarator design is about optimising trade-offs

- First a plasma equilibrium must be constructed with desired aspect ratio, pressure and rotational transform
- Quasi-symmetric or quasi-omnigenous configurations minimise neoclassical transport

¹³See e.g. work by Pavlos Xanthopoulos using GS2

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- The plasma must avoid large-scale instabilities
- The Pfirsch-Schüter and Bootstrap currents are calculated. These are usually minimised to have maximum control over the plasma configuration
- In the last couple of years it has become possible to start optimising anomalous (turbulent) transport¹³

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- In the last couple of years it has become possible to start optimising anomalous (turbulent) transport¹³
- A design of coils is produced which create the desired field
- These coils may not be practical, so modify the design
- Repeat until an optimised design is produced

H.E.Mynick, Phys. Plasmas 13, 058102 (2006)

¹³See e.g. work by Pavlos Xanthopoulos using GS2

There were several problems with Stellarators

- Complicated coil configurations need to be very precise $(\sim 1 \text{mm})$, and are difficult to design and expensive to build. They must be capable of carrying Mega-Ampéres of current, and withstanding huge forces
- Generally, stellarator configurations cannot be varied to the extent that tokamaks can. This makes experimentation more difficult
- Achieving good particle confinement is more difficult in stellarators than tokamaks
- So far, stellarators have not reached the same performance (pressure β and density) as tokamaks
- The divertor and heat-handling regions have a more complicated geometry than tokamaks, complicating the engineering

- Stellarators are intrinsically steady-state, as there is no need to drive a plasma current
- Lack of plasma current removes a large class of instabilities which we'll see later in tokamaks
- Because the rotational transform and position of the plasma is set by external coils and not by currents in the plasma, stellarators do not suffer violent disruptions
- Stellarators have a much greater range of designs than tokamaks, potentially allowing greater optimisation of performance
- With the construction of Wendelstein 7-X, new concepts such as quasi-symmetry, and the interest in 3D fields in tokamaks, there is renewed interest in stellarator research.