

# Probability Distribution of Substituted Titanium in $RT_{12}$ (R = Nd and Sm; T = Fe and Co) Structures

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We investigated the atomic fill site probability distributions across supercell structures of  $RT_{12-x}Ti$  (R = Nd and Sm; T = Fe and Co). We use a combined molecular dynamics and Boltzmann distribution approach to extrapolate the probability distributions for Ti substitution from lower to higher temperatures with an equilibrium condition to assess how temperature affects the predictability of the structures' fill path. It was found that the Nd- and Sm-based Fe systems have the highest filling probability path at lower temperatures, but the cohesive energy change due to Ti substitution in Sm- and Nd-based crystals indicates that a more stable system could be achieved with a combination of Co and Fe in the transition metal site.

**Index Terms**—1:12 phase, cohesive energy, probability distribution.

## I. INTRODUCTION

PERMANENT magnetic materials have been an important area of research for the last century [1], starting with high carbon steels in the early 1900s and moving on to high-performance rare earth magnets near the end of the century. As their properties have improved, their application has grown and they are now used in a wide variety of products such as printers, hard disks, MRIs, and electrical engines. Of these areas of application, their use in electrical engines is the most important for the realization of a future that runs entirely on renewable energy sources. Their use in the engines of electric vehicles and renewable energy technologies such as wind turbines is of utmost importance to these devices' efficient performance.

The performance of a high-density permanent magnet can be classified by its maximum energy product ( $BH_{max}$ ), which is governed by its remanent magnetization, and coercivity. As these properties are temperature-dependent and energy applications of magnets operate at high temperatures, e.g., electrical engines operate at 450–475 K, it is important to understand the fundamental morphological and chemical properties that govern this temperature dependency.

The current permanent magnetic material used in electrical engines,  $Nd_2Fe_{14}B$ , has a curie temperature of 585 K as measured by Sagawa *et al.* [2], but can be improved

through substitution of neodymium with dysprosium to reach higher Curie temperature, and this is the predominant method currently used to improve the properties of  $Nd_2Fe_{14}B$  at high temperatures. However, due to the scarcity and therefore prohibitively high cost of dysprosium, as well as its potentially tenuous supply [3], there is a great deal of pressure to find new permanent magnetic materials made of abundant and hence cheaper constituents that have similar magnetic properties but higher Curie temperature.

One of the most promising of these materials is the  $RT_{12}$  (R = rare earth and T = transition metal) phase, which forms in the  $ThMn_{12}$  structure. The phases main problem is its intrinsic instability in binary form, meaning it must be stabilized with a ternary element to form an  $RT_{12-x}M_x$  structure (M = Si, Ti, V, Cr, Mo, or W). It was found by De Mooij and Buschow [4] that of the possible phases, the  $RFe_{12-x}M_x$  phase was the most promising due to the high magnetic moment and anisotropy provided by iron. Furthermore, investigation of this phase with M = Ti by Yang *et al.* [5] found that nitrogenation of these structures causes significant changes to their magnetocrystalline anisotropy, and via this method, their magnetic properties could be significantly improved. Of the structures, investigated  $NdFe_{11}TiN$  was thought to be the most promising with a Curie temperature of 740 K and estimated  $BH_{max}$  of 455 kJ/m<sup>3</sup>, which compares well to  $Nd_2Fe_{14}B$ 's theoretical  $BH_{max}$  of ~500 kJ/m<sup>3</sup> and Curie temperature of 585 K [6].

Recent computational investigation of this phase by Miyake *et al.* [7] has shown that titanium substitution changes crystal electric field parameter  $A_{20}$  from -83 K in  $NdFe_{12}$  to +54 K in  $NdFe_{11}Ti$ . Nitrogenation of this structure further increases  $A_{20}$  to +439 K. Titanium substitution while stabilizing the structure also causes a large loss of spin magnetic

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TABLE I  
LATTICE CONSTANT COMPARISON

Structure	Expected			Calculated		
	a	b	c	a	b	c
NdFe <sub>11</sub> Ti	8.574	8.574	4.907	8.554	8.553	4.853
SmFe <sub>11</sub> Ti	8.557	8.557	4.800	8.482	8.494	4.814
SmCo <sub>11</sub> Ti	8.426	8.426	4.741	8.508	8.513	4.821

Shows a comparison of the expected and calculated values for the various structures lattice parameters. All values are given in Angstrom. The expected values for NdFe<sub>11</sub>Ti and SmFe<sub>11</sub>Ti can be found in [4], the expected values of SmCo<sub>11</sub>Ti can be found in [5].

moment per formula unit of:  $-4.90 \mu_B$  from NdFe<sub>12</sub> to NdFe<sub>11</sub>Ti and  $-5.16 \mu_B$  from NdFe<sub>12</sub>N to NdFe<sub>11</sub>TiN, this is due to Ti aligning anti-parallel to the internal magnetization and decreasing the magnetic moment of the surrounding iron atoms. Therefore, it is important that titanium substitution is kept to a minimum and that its behavior inside the structure is well understood.

This paper is concerned with the investigation of the RT<sub>12-x</sub>Ti<sub>x</sub> (R = Sm and Nd; T = Fe and Co) phases' structural properties and how they change with titanium substitution. We use molecular dynamics with Morse potentials and Boltzmann statistics to investigate how replacement of the transition element with a tertiary element changes the calculated cohesive energy of the structure at low titanium at%, as well as investigating the probability distribution of titanium over the atom positions within the structure.

## II. METHODOLOGY

In order to calculate the structural properties of the RT<sub>12-x</sub>Ti<sub>x</sub> phases, we use molecular dynamics, which uses the classical equations of motion with parameterized force fields to predict the structure of physical systems [8]. As described in [9] interatomic potentials for metals are used to simulate atom interactions in our investigated system. We use Morse [10] and modified embedded atom models, which are derived from ab initio and validated with lattice constants from experiments and the literature. Our calculated lattice constants for SmFe<sub>11</sub>Ti, NdFe<sub>11</sub>Ti, and SmCo<sub>11</sub>Ti were in agreement with those found in [5], [5], and [11] to within <2% (see Table I), while the Ti replacements followed the expected pattern set out by De Mooij and Buschow [4].

The metallic phase is modeled with a Morse potential of the form

$$\Phi_{sr}(r_{ij}) = D_{ij}[(1 - e^{-\beta_{ij}(r-r_0)})^2 - 1] \quad (1)$$

where  $\Phi_{sr}(r_{ij})$  is the potential energy between atoms  $i$  and  $j$ ,  $D_{ij}$  is the disassociation energy of the bond,  $\beta_{ij}$  is a variable parameter that can be determined from spectroscopic data,  $r$  is the distance between the atoms, and  $r_0$  is the equilibrium bond distance. The potential energy of the system was minimized via the Newton-Raphson method in General Utility Lattice Program (GULP) [8].

The set of potentials pertaining to Nd in the NdFe<sub>12-x</sub>Ti<sub>x</sub> simulation are shown graphically in Fig. 1.

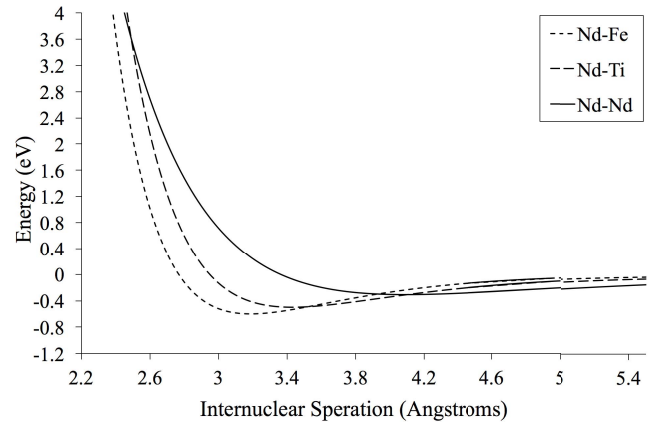


Fig. 1. Interatomic potentials for Nd-Fe, Nd-Ti, and Nd-Nd.

Using these potentials, energy minimization calculations are performed on the investigated structures at constant pressure until they reach local energy minima; the structural properties as well as the cohesive energy of this optimized structure are then output, with the minimum energy structure being used to inform the next round of calculations. In this way, titanium is permuted through the structure up to the desired stoichiometric percentage.

Using the output data and basing on energy, we calculate the probability ratios for each position being filled at increasing stoichiometric Ti at% up to ~4%. The ratios are based off of Boltzmann statistics and modeled on the Boltzmann distribution equation [12]

$$p(r) = \frac{e^{\frac{-E_r}{k_B T}}}{\sum_i e^{\frac{-E_i}{k_B T}}} \quad (2)$$

where  $p(r)$  is the probability of state  $r$ ,  $E_r$  is the energy of state  $r$ ,  $k_B$  is Boltzmann's constant, and  $T$  is the temperature in kelvin. These probabilities are then normalized by the probability of the minimum energy position, which gives probability ratios that can be calculated by the following equation:

$$\frac{p(\text{state2})}{p(\text{state1})} = e^{\frac{E_1 - E_2}{k_B T}} \quad (3)$$

The ratios are further normalized by the summation of all ratios to give each position percentage probability at a particular Ti at%. While the simulations were run at 0 K, it has been assumed that probabilities at higher temperatures can be obtained by scaling with  $k_B T$  and making the assumption that these systems have been left to find equilibrium, so that necessarily the most probable position will be filled by the replacing titanium.

## III. RESULTS

Simulations calculating Ti atom distribution within singular unit cells of the three investigated structures showed clear differences between the probabilities of the  $8i$ ,  $8j$ , and  $8f$  Wyckoff position sets in the ThMn<sub>12</sub> phase structure. The  $8i$  position set has the highest probability for replacement

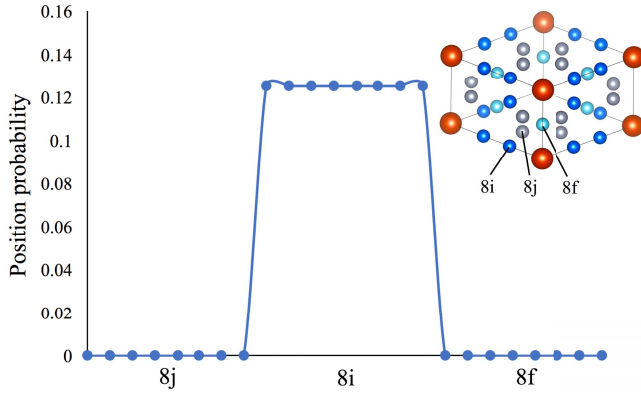


Fig. 2. Graph showing the probability distribution for Ti across the  $8i$ ,  $8j$ , and  $8f$  sets of atomic positions at 300 K. Singular unit cell of the 1:12 phase structure (top right). The atoms sets are labeled and colored by position; dark blue is the  $8i$  position set, gray is the  $8j$  position set, and light blue is the  $8f$  position set.

followed by the  $8j$  and  $8f$  sets; this is in agreement with the results from Miyake *et al.* [7]. This probability distribution is shown in Fig. 2, along with a diagram of the 1:12 phase structure noting the three sets of Wyckoff positions.

Due to the difference in probability between the position sets at 300 K being of the order  $10^{19}$  and  $10^{32}$  for  $8i/8j$  and  $8i/8f$ , respectively, it is reasonable to assume that at  $<4\%$  Ti at%, the only positions of significance will be those in the  $8i$  position set, and this is exactly what was seen by De Mooij and Buschow [4]. All future simulations, therefore, disregard all but the  $8i$  positions in an effort to improve computational efficiency.

Supercell structures were investigated in order to decrease the Ti percentage in the structure to  $<4\%$  and down to  $\sim 1$  Ti at%. The results of these simulations are given below. The  $8i$  positions within these supercell structures are given in Table II.

#### A. NdFe<sub>12</sub>

Titanium replacements align around a singular Nd atom with the first substitution designating which of the atoms it will be, for example, the first position may be 5. The first substitution is followed by a second which goes with equal probability to one of the next two nearest neighbors that surround the Nd atom, positions 21 and 29 in the case of 5 being the first substitution. This repeats up to  $\sim 4$  Ti at% at which point the structure has a layout analogous to that shown in Fig. 3(a). The path taken to the pictured structure is (position) 5, 21, 13, and 29.

#### B. SmCo<sub>12</sub>

The first two titanium replacements in this unit cell follow the same pattern as those in NdFe<sub>12</sub> and start by surrounding a samarium atom; however, on the third substitution, the titanium replacement fills an analogous position to the one it would have done in NdFe<sub>12</sub> but in a different unit cell. The unit cell the replacing atom goes to is dependent on which similar position it would have filled. For example,

TABLE II  
POSITION UNIT CELL AND FRACTIONAL COORDINATES

Position	Unit cell	a	b	c
1	[0,0,0]	0.1784	0	0
2	[0,0,0] [0,1,0]	0.1784	0.5	0
3	[1,0,0]	0.6784	0	0
4	[1,0,0] [1,1,0]	0.6784	0.5	0
5	[0,0,0]	0.4284	0.25	0.5
6	[0,1,0]	0.4284	0.75	0.5
7	[1,0,0]	0.9284	0.25	0.5
8	[1,1,0]	0.9284	0.75	0.5
9	[0,0,0]	0.3216	0	0
10	[0,0,0] [0,1,0]	0.3216	0.5	0
11	[1,0,0]	0.8216	0	0
12	[1,0,0] [1,1,0]	0.8216	0.5	0
13	[0,0,0]	0.0716	0.25	0.5
14	[0,1,0]	0.0716	0.75	0.5
15	[1,0,0]	0.5716	0.25	0.5
16	[1,1,0]	0.5716	0.75	0.5
17	[0,0,0]	0	0.3216	0
18	[0,1,0]	0	0.8216	0
19	[0,0,0] [1,0,0]	0.5	0.3216	0
20	[0,1,0] [1,1,0]	0.5	0.8216	0
21	[0,0,0]	0.25	0.0716	0.5
22	[0,1,0]	0.25	0.5716	0.5
23	[1,0,0]	0.75	0.0716	0.5
24	[1,1,0]	0.75	0.5716	0.5
25	[0,0,0]	0	0.1784	0
26	[0,1,0]	0	0.6784	0
27	[0,0,0]	0.5	0.1784	0
28	[0,1,0] [1,1,0]	0.5	0.6784	0
29	[0,0,0]	0.25	0.4284	0.5
30	[0,1,0]	0.25	0.9284	0.5
31	[1,0,0]	0.75	0.4284	0.5
32	[1,1,0]	0.75	0.9284	0.5

Lists all 32  $8i$  positions in a  $2 \times 2$  supercell of the 1:12 phase structure, the unit cell they occupy, and their fractional coordinates within the supercell.

if positions 5 then 21 are filled, the third position could be 14 or 31, which are similar to positions 15 and 29, respectively. The final substitution surrounds a further none similar samarium atom, and when extending the cell boundaries, it becomes clear that the titanium has substituted itself such that it forms lines that run through the solid roughly along the  $[110]$  or  $[-110]$  direction. The direction of the line is dependent on the second atom substitution, and the  $[110]$  direction structure at  $\sim 4$  Ti at% is shown in Fig. 3(b). The path taken to the pictured structure is (position) 1, 18, 12, and 25.

#### C. SmFe<sub>12</sub>

The first three titanium replacements follow the same pattern seen in SmCo<sub>12</sub> and align themselves around a singular Sm atom before filling a similar position that is analogous to one that would have been filled in NdFe<sub>12</sub>. However, on the final atom, rather than spreading out evenly between the unit cells as in SmCo<sub>12</sub>, the substitution fills the final space surrounding

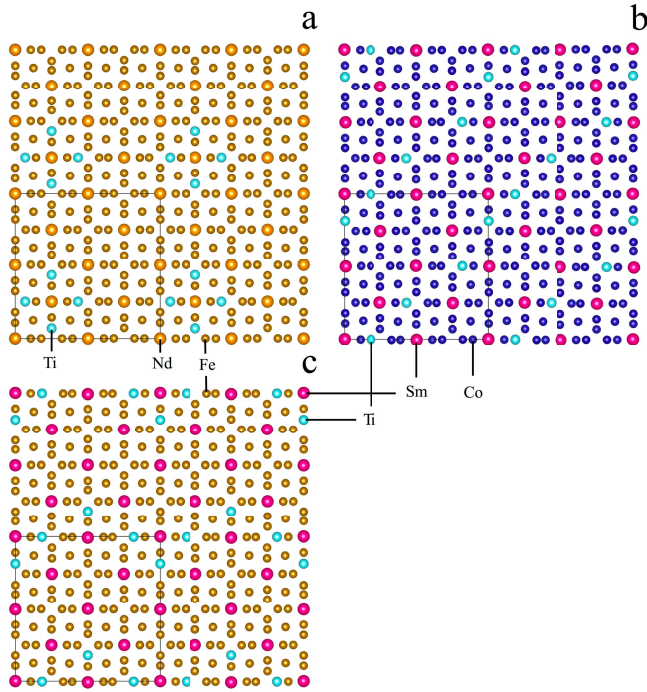


Fig. 3. Minimum energy structures of the investigated  $2 \times 2$  supercells at  $\sim 4$  Ti at%. The black box seen in the bottom left corner of each unit cell encloses one supercell structure. (a)  $\text{NdFe}_{12-x}\text{Ti}_x$ . (b)  $\text{SmCo}_{12-x}\text{Ti}_x$  in [110] direction. (c)  $\text{SmFe}_{12-x}\text{Ti}_x$  in [100] direction. In all diagrams, Ti is light blue, Nd is light orange, Fe is dark orange, Sm is pink, and Co is dark blue.

the first Sm which it has not already similarly filled elsewhere in the structure. For example, if positions 5, 21, and 14 are filled, then the final fill position would be 13. This substitution layout forms a zig-zag pattern moving in the [100] or [010] direction, with the direction of the pattern dependent on the third substitution. The final structure in the [100] direction at  $\sim 4$  Ti at% is shown in Fig. 3(c). The path to get to the pictured structure is positions 1, 18, 27, and 11.

The three structures probability distributions predict that they behave the same way at or below  $\sim 2$  Ti at%, with divergent distributions occurring at  $\sim 3$  Ti at% and above for the Nd- and Sm-based systems and at  $\sim 4$  Ti at% for the Co- and Fe-based Sm systems.

However, although all the distributions indicate that the structures will share behavior at or below  $\sim 2$  Ti at%, at higher temperatures, the probability that the expected permutation occurs starts to differ between structures. For example, at 1 K, the probability, the expected permutation occurs is 100% for all structures at  $\sim 2$  Ti at%; however, at 300 K, this drops to 42.6% for  $\text{SmFe}_{12}$ , 38.1% for  $\text{NdFe}_{12}$ , and 15.4% for  $\text{SmCo}_{12}$ . The large disparity between the Fe- and Co-based systems indicates that having Fe as the transition element makes the structure more predictable.

As these probability distributions are given at each substitution point in a permutation path, they can be aggregated across all permutations, to give each positions percentage of the total probability at a given Ti at% for a range of temperatures. Summing the probabilities of all the positions at each temperature gives a percentage value that indicates how closely the structure adheres to the permutation paths

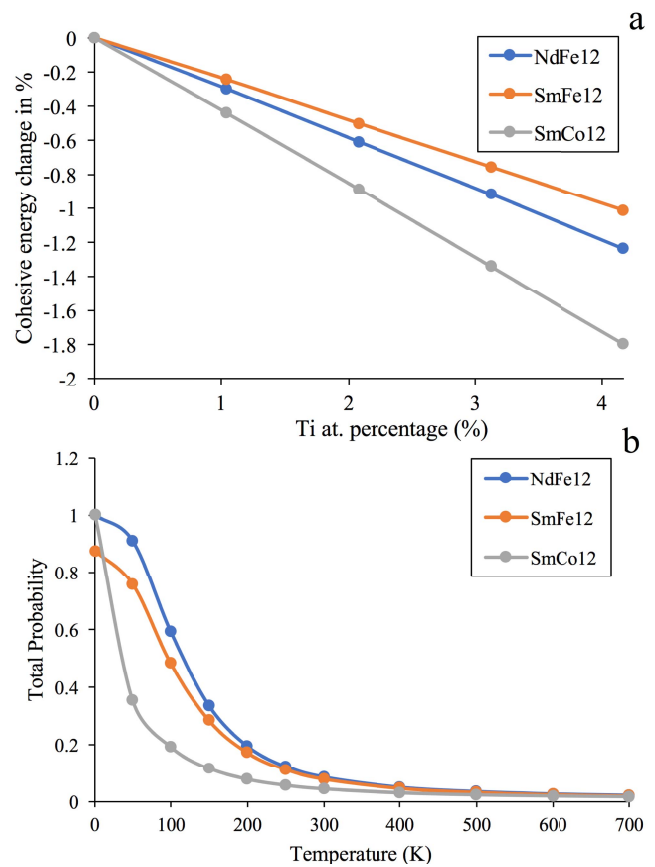


Fig. 4. (a) Graph of the percentage change in cohesive energy against Ti at% for  $\text{NdFe}_{12}$ ,  $\text{SmFe}_{12}$ , and  $\text{SmCo}_{12}$ . (b) Graph of the total probability contained by the minimum energy criteria at the fourth Ti substitution extrapolated from 0 up to 700 K for  $\text{NdFe}_{12}$ ,  $\text{SmFe}_{12}$ , and  $\text{SmCo}_{12}$ .

chosen by the simulations search criteria (minimum energy), which acts as a measure of the reliability of its behavior at that temperature. This was used to compare the reliability of the investigated structures at  $>2$  Ti at%, and a graph of the aggregated total probabilities for each structure against temperature is included in Fig. 4(b).

It can be seen from this graph that as noted previously, the Fe-based systems retain more of their total probability than that of the Co-based systems at higher temperature, which indicates that they will follow the permutation paths more reliably, and hence are more predictable structures. This predictability becomes important when trying to microengineer the structure.

A graph of the percentage change in cohesive energy of these structures against Ti at% is also given in Fig. 4(a). As can be seen from this graph,  $\text{SmCo}_{12}$  gains much larger percentage change in energy per Ti substitution, and therefore if it follows the permutation path exactly, it is likely the most stable of the investigated structures.

#### IV. CONCLUSION

As can be seen in Fig. 4(a), the average percentage gain in cohesive energy per Ti substitution is  $-0.45\%$  for  $\text{SmCo}_{12}$  and  $-0.31\%$  and  $-0.25\%$  for  $\text{NdFe}_{12}$  and  $\text{SmFe}_{12}$ , respectively, indicating that  $\text{SmCo}_{12}$  is the most stable when substituted with Ti. However, as can be seen from Fig. 4(b),  $\text{SmCo}_{12}$

has a very low probability of following the permutation path that gives these percentage gains in cohesive energy, even at relatively low temperatures, whereas the Fe-based systems retain a greater percentage of their probabilities. Therefore, a hybrid structure using both Fe and Co as the transition metal in the 1:12 phase may be a prudent way to solve both the need for greater gains in stability per Ti substitution, and the need for a predictable structure.

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#### REFERENCES

- [1] J. D. Livingston, “The history of permanent-magnet materials,” *JOM*, vol. 42, no. 2, pp. 30–34, Feb. 1990.
- [2] M. Sagawa, S. Hirosawa, H. Yamamoto, S. Fujimura, and Y. Matsuura, “Nd-Fe-B permanent magnet materials,” *Jpn. J. Appl. Phys.*, vol. 26, no. 6, p. 785, 1987.
- [3] M. Humphries, *Rare Earth Elements the Global Supply Chain*. Washington, DC, USA: Congressional Research Service, 2013.
- [4] D. B. De Mooij and K. H. J. Buschow, “Some novel ternary ThMn<sub>12</sub>-type compounds,” *J. Less Common Metals*, vol. 136, no. 2, pp. 207–215, 1988.
- [5] Y.-C. Yang, X.-D. Zhang, L.-S. Kong, Q. Pan, and S.-L. Ge, “Magnetocrystalline anisotropies of RTiFe<sub>11</sub>N<sub>x</sub> compounds,” *Appl. Phys. Lett.*, vol. 58, no. 18, p. 2042, 1991.
- [6] S. Hirosawa, Y. Matsuura, H. Yamamoto, S. Fujimura, M. Sagawa, and H. Yamauchi, “Magnetization and magnetic anisotropy of R<sub>2</sub>Fe<sub>14</sub>B measured on single crystals,” *J. Appl. Phys.*, vol. 59, no. 3, p. 873, 1986.
- [7] T. Miyake, K. Terakura, Y. Harashima, H. Kino, and S. Ishibashi, “First-principles study of magnetocrystalline anisotropy and magnetization in NdFe<sub>12</sub>, NdFe<sub>11</sub>Ti, and NdFe<sub>11</sub>TiN,” *J. Phys. Soc. Jpn.*, vol. 83, no. 4, p. 043702, 2014.
- [8] J. D. Gale, “GULP: A computer program for the symmetry-adapted simulation of solids,” *J. Chem. Soc., Faraday Trans.*, vol. 93, no. 4, p. 629, 1997.
- [9] S. C. Westmoreland *et al.*, “Multiscale model approaches to the design of advanced permanent magnets,” *Scripta Mater.*, vol. 148, pp. 56–62, Apr. 2018.
- [10] P. M. Morse, “Diatomic molecules according to the wave mechanics. II. Vibrational levels,” *Phys. Rev.*, vol. 34, no. 1, p. 57, 1929.
- [11] W. Q. Wang *et al.*, “Structural and magnetic properties of RCo<sub>12-x</sub>Ti<sub>x</sub> (R = Y and Sm) and YFe<sub>12-x</sub>Ti<sub>x</sub> compounds,” *J. Phys. D, Appl. Phys.*, vol. 34, no. 3, p. 307, 2001.
- [12] S. J. Blundell and K. M. Blundell, *Concepts in Thermal Physics*. New York, NY, USA: Oxford Univ. Press, 2006, p. 37.