

Lecture 10

Moving wings and real aircraft

So far we have considered flow around a stationary wing, and seen that there must be circulation Γ in order to keep the flow smooth.

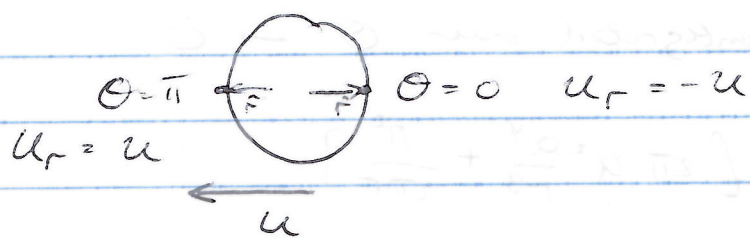
For flow at speed u past a stationary wing

$$\phi = u \left(r + \frac{a^2}{r} \right) \cos \theta + \frac{\Gamma \theta}{2\pi}$$

For a wing moving at speed u through a stationary fluid

$$\phi = u \frac{a^2}{r} \cos \theta + \frac{\Gamma \theta}{2\pi}$$

check $u_r = \frac{\partial \phi}{\partial r} = -u \frac{a^2}{r^2} \cos \theta$



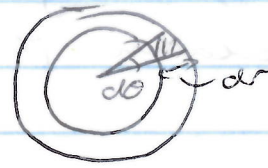
$$u_\theta = \frac{1}{r} \frac{\partial \phi}{\partial \theta} = -u \frac{a^2}{r^2} \sin \theta + \frac{\Gamma}{2\pi r}$$

What is the kinetic energy of the fluid?

$$k.E. = \int \frac{1}{2} \rho |u|^2 dV = \int \frac{1}{2} \rho (u_r^2 + u_\theta^2) dV$$

Volume element

$$dV = r dr d\theta$$



Integrating over all θ , and from $r=a$ to $r \rightarrow \infty$

$$k.E. = \int_a^\infty dr \int_0^{2\pi} d\theta \frac{1}{2} \rho \left[\left(-u \frac{a^2}{r^2} \cos\theta \right)^2 + \left(-u \frac{a^2}{r^2} \sin\theta + \frac{\Gamma}{2\pi r} \right)^2 \right] r$$

$$\text{note: } \cos^2\theta + \sin^2\theta = 1$$

$$= \int_a^\infty dr \int_0^{2\pi} d\theta \frac{1}{2} \rho \left[u^2 \frac{a^4}{r^3} - 2u \frac{a^2}{r} \sin\theta \frac{\Gamma}{2\pi r} + \frac{\Gamma^2}{4\pi^2 r} \right]$$

$\sin\theta$ integrated over $\theta \rightarrow 0$

$$k.E. = \int_a^\infty dr \frac{1}{2} \rho \left[2\pi u^2 \frac{a^4}{r^3} + \frac{\Gamma^2}{2\pi r} \right]$$

$$= \frac{1}{2} \rho \left[-\pi u^2 \frac{a^4}{r^2} + \frac{\Gamma^2}{2\pi} \ln r \right]_a^\infty$$

$$\underbrace{\frac{1}{2} \rho \pi a^2 u^2}_{M^*}$$

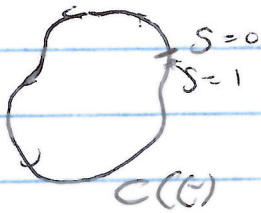
$\rightarrow \infty!$ Depends on boundary conditions.

effective Mass of fluid dragged along by moving body

10.2

Kelvin's circulation theorem

$$\frac{d}{dt} \int_{C(t)} \underline{u} \cdot d\underline{x} = \int_{C(t)} \frac{D\underline{u}}{Dt} \cdot d\underline{x}$$



$$\underline{x} = \underline{x}(s, t)$$

$$d\underline{x} = \frac{\partial \underline{x}}{\partial s} ds$$

$$\frac{d}{dt} \int_{C(t)} \underline{u} \cdot d\underline{x} = \frac{d}{dt} \int_0^1 \frac{\partial}{\partial t} \left(\underline{u} \cdot \frac{\partial \underline{x}}{\partial s} \right) ds$$

↑
fixed s

$$\int_0^1 \frac{\partial \underline{u}}{\partial t} \cdot \frac{\partial \underline{x}}{\partial s} ds + \int_0^1 \underline{u} \cdot \frac{\partial}{\partial s} \left(\frac{\partial \underline{x}}{\partial t} \right) ds$$

$$\frac{d}{dt} \oint_{C(t)} \underline{u} \cdot d\underline{x} = \oint \frac{D\underline{u}}{Dt} \cdot d\underline{x} + \oint \underline{u} \cdot \frac{d(d\underline{x})}{dt}$$

↑
change of \underline{u}
following the fluid

$$\frac{D\underline{u}}{Dt} = -\nabla \left(\frac{P}{\rho} + \chi \right)$$

$$\begin{aligned} \Rightarrow \frac{d}{dt} \oint_{C(t)} \underline{u} \cdot d\underline{x} &= - \oint \nabla \left(\frac{P}{\rho} - \frac{1}{2} u^2 + \chi \right) \cdot d\underline{x} \\ &= - \left[\frac{P}{\rho} - \frac{1}{2} u^2 + \chi \right]_C \\ &= 0 \end{aligned}$$

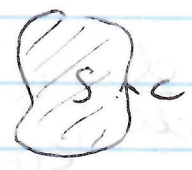
- Does not need to be incompressible.
- Does not need to be 'simply connected'

using Stokes' theorem

$$\oint_C \mathbf{u} \cdot d\mathbf{x} = \int_S \underline{\omega} \cdot \underline{n} \, dS$$

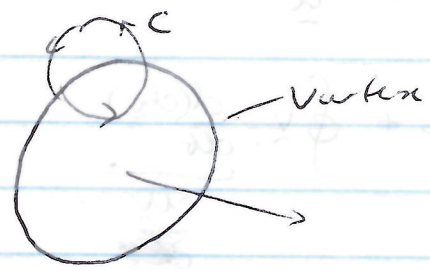
Inviscid, incompressible flow

If $\underline{\omega} = 0$ initially, then it is always zero



→ Cauchy Lagrange theorem

Shown easily in 2D, in 3D use Kelvin's circulation



Vortex moves with fluid

→ persistence of vortex rings

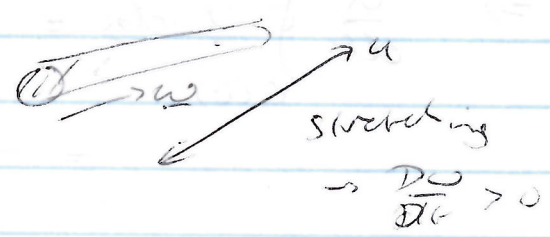
Vortex stretching

$$\frac{D\underline{\omega}}{dt} = (\underline{\omega} \cdot \nabla) \mathbf{u}$$

e.g. 2D

$$\underline{\omega} = (0, 0, \omega_z)$$

$$\frac{\partial \omega_z}{\partial t} = \omega_z \frac{\partial u}{\partial z}$$



stretching

$$\rightarrow \frac{D\omega}{Dt} > 0$$

$$\frac{d}{dt} \int_S \underline{\omega} \cdot \underline{n} \, dS = 0$$

⇒ shrinking



increases ω

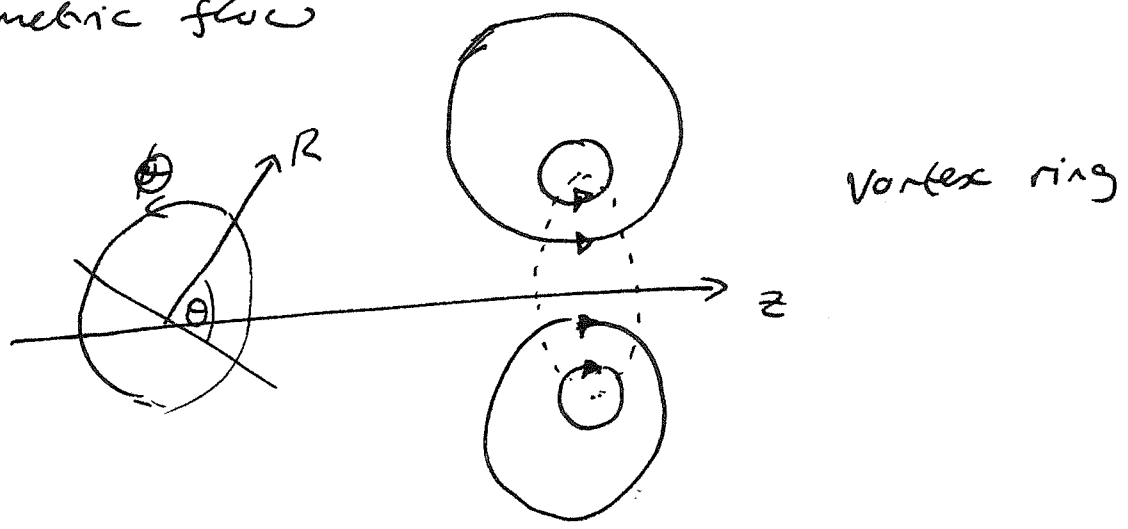
e.g. tornadoes

10.3

Vorticity equation in cylindrical coordinates

$$\frac{D\omega}{Dt} = (\omega \cdot \nabla) \underline{u}$$

axisymmetric flow



If flow is constant in θ e.g. vortex ring

then
$$\underline{u} = u_R(R, z, t) \hat{e}_R + u_z(R, z, t) \hat{e}_z$$

By the Kelvin's circulation theorem

→ vorticity moves with flow so that the vortex ring keeps its vorticity as it moves

$$\omega = \nabla \times \underline{u}$$

only non-zero component is

$$\omega = \omega_\theta \hat{e}_\theta = \left(\frac{\partial u_R}{\partial z} - \frac{\partial u_z}{\partial R} \right) \hat{e}_\theta$$

$$\frac{D\omega}{Dt} = \frac{\partial \omega}{\partial t} + \underline{u} \cdot \nabla \omega = (\omega \cdot \nabla) \underline{u}$$

$$\frac{\partial \omega_\theta}{\partial t} \hat{e}_\theta + \underline{u} \cdot \nabla (\omega_\theta \hat{e}_\theta) = \omega_\theta \frac{1}{R} \frac{\partial}{\partial \theta} (u_R \hat{e}_R + u_z \hat{e}_z)$$

using $\frac{\partial \hat{e}_r}{\partial \theta} = \hat{e}_\theta$

$$\frac{\partial \omega_\theta}{\partial t} \hat{e}_\theta + \underline{u} \cdot \nabla (\omega_\theta \hat{e}_\theta) = \frac{\omega_\theta}{R} u_r \hat{e}_\theta$$

using $\frac{\partial \hat{e}_\theta}{\partial r} = 0$, $\frac{\partial \hat{e}_\theta}{\partial z} = 0$ and $u_r = \underline{u} \cdot \nabla R$

Divide through by R :

$$\frac{\partial}{\partial t} \left(\frac{\omega_\theta}{R} \right) \hat{e}_\theta + \frac{1}{R} \underline{u} \cdot \nabla \omega_\theta \hat{e}_\theta - \hat{e}_\theta \frac{\omega_\theta}{R^2} \underline{u} \cdot \nabla R = 0$$
$$\underbrace{\hspace{15em}}_{\underline{u} \cdot \nabla \left(\frac{\omega_\theta}{R} \right) \hat{e}_\theta}$$

therefore

$$\frac{\partial}{\partial t} \left(\frac{\omega_\theta}{R} \right) + \underline{u} \cdot \nabla \left(\frac{\omega_\theta}{R} \right) = 0$$

or

$$\underline{\underline{\frac{D}{Dt} \left(\frac{\omega_\theta}{R} \right) = 0}}$$

hence the vorticity of a smoke ring moves with the fluid, and changes in proportion to R .

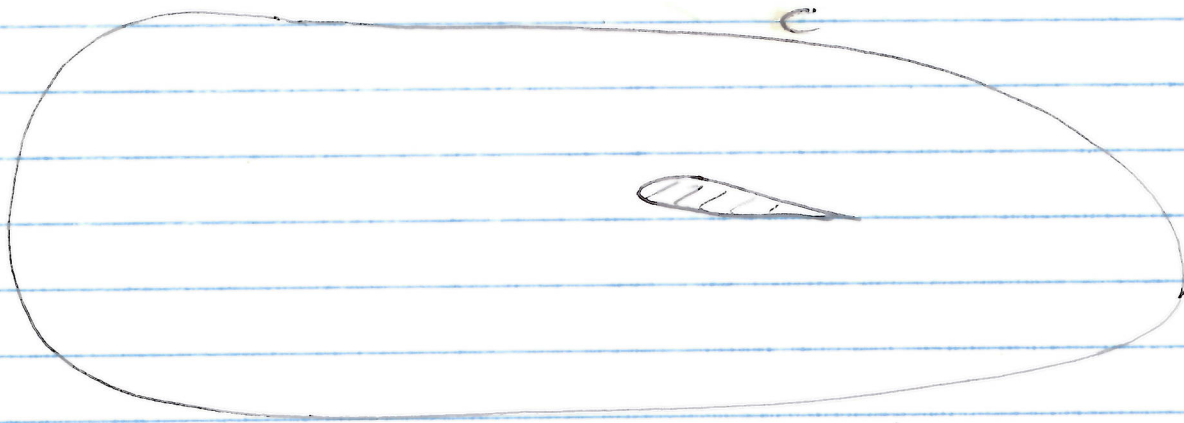
Starting vortices

~~Kelvin's~~ Kelvin's theorem: In the absence of viscosity, if $C(t)$ is a curve that consists of the same fluid particles as time proceeds, then

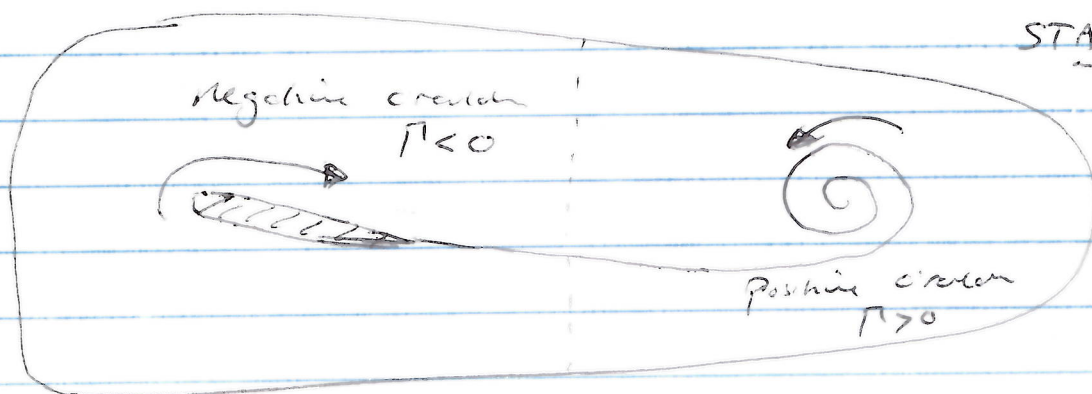
$$\Gamma = \int_{C(t)} \underline{u} \cdot d\underline{x} \text{ is independent of time}$$

Note: Does not depend on incompressibility, does not require surface to be only within the fluid

Consider a wing initially at rest $\Gamma = \int_{C(t)} \underline{u} \cdot d\underline{x} = 0$



How does the negative circulation around the wing occur?

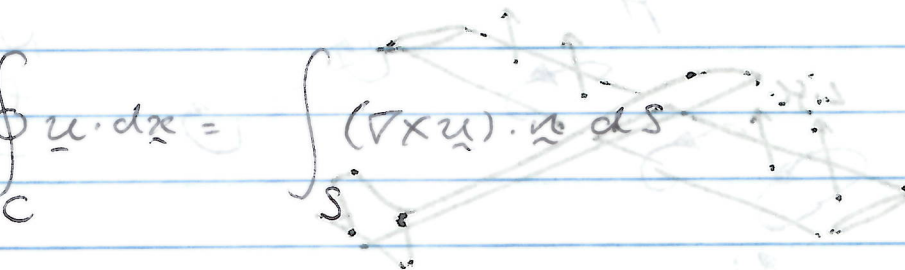
STARTING VORTEX

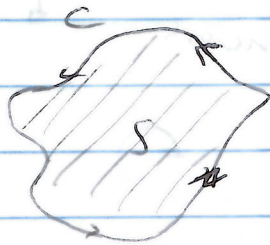
By Kelvin's theorem, if there is a negative circulation around the wing, then there must have been a vortex shed from the wing with positive circulation.

10.5

3D wings ~~cannot generate a circulation~~ ~~the circulation of a lifting surface is constant~~
 The circulation of a lifting surface is constant in 3D.

Stoke's theorem says:

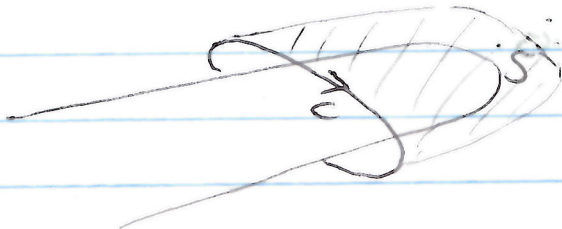
$$\oint_C \underline{u} \cdot d\underline{x} = \int_S (\nabla \times \underline{u}) \cdot \underline{n} \, dS$$




In 2D, ~~flow~~ irrotational flow, $\nabla \times \underline{u} = 0$ and so $\int_C \underline{u} \cdot d\underline{x} = 0$ for any closed curve C.

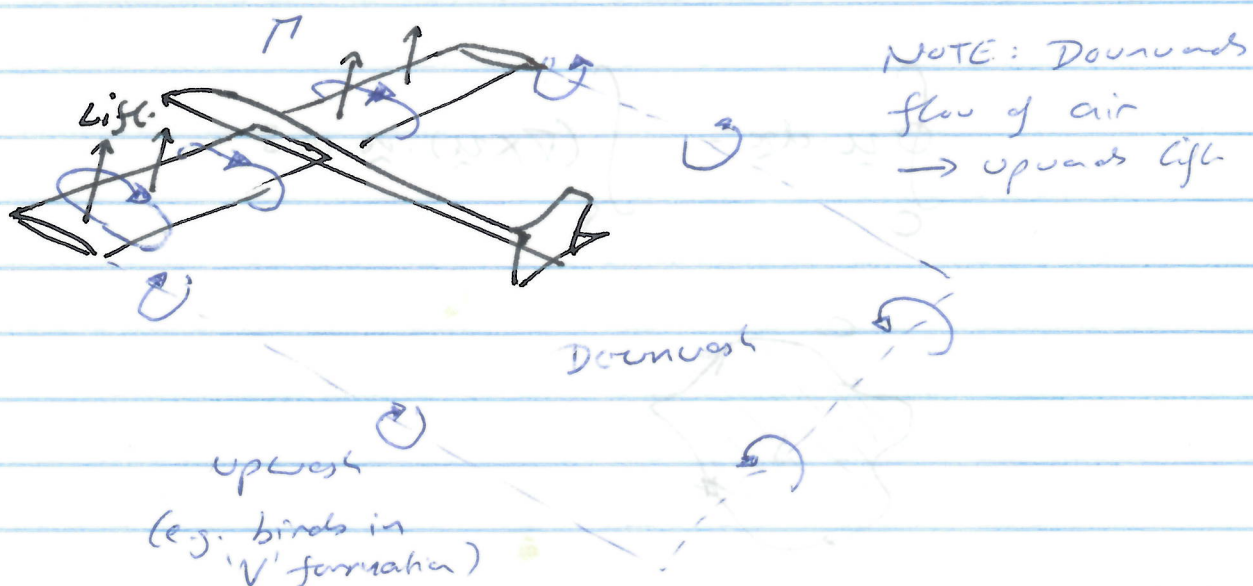
$\Gamma = \oint_C \underline{u} \cdot d\underline{x} = 0$ except where the surface encloses the wing.

In 3D we can always create a surface which lies entirely in the fluid. ~~is necessary in direction of circulation~~ ~~circulation must be zero for the air - a trailing vortex~~



From Stoke's theorem, if there is any circulation (and so lift) then there must be vorticity $\nabla \times \underline{u} \neq 0$
 \Rightarrow This is seen as a Trailing vortex

The combination of a starting vortex and trailing vortex produces a 'horseshoe vortex' behind an aircraft in 3D



In reality the lift generated varies along the length of the wing. Whenever the circulation (lift) varies, vorticity is shed from the wing (lifting line theory)

Shedding of vorticity is necessary in 3D for lift. The aircraft must do work on the air → induced drag even when no viscosity.